

1 H_∞ CONTROL FOR STOCHASTIC SYSTEMS WITH
2 DISTURBANCE PREVIEW *

3 HONGXIA WANG[†], MINYUE FU[‡], AND HUANSUI ZHANG[§]

4 **Abstract.** The paper considers the H_∞ control problem for stochastic systems with disturbance
5 preview, which is very challenging since it involves the preview problem and multiplicative noise
6 simultaneously. The H_∞ control problem for deterministic systems with disturbance preview was
7 once listed as one of the 53 open problems in mathematical and control and its methods can not
8 be generalized to solve the corresponding stochastic problem because of the essential differences of
9 the two classes of systems. Using the projection principle in indefinite space, we give a necessary
10 condition of the solvable H_∞ preview control problem by using a pair of variables. The necessary
11 condition is very useful for solving the minimax problem. An inertia condition of matrices, as
12 the necessary and sufficient condition under which the H_∞ control for stochastic linear systems is
13 solvable, is also proposed and testified. This condition generalizes the results for H_∞ control for
14 deterministic systems with disturbance preview. Our results are demonstrated via a quarter vehicle
15 active suspension system.

16 **Key words.** stochastic system, disturbance attenuation, minimax problem, H_∞ preview control

17 **AMS subject classifications.** 39A06, 93E15, 93D15

18 **1. Introduction.** Disturbance attenuation has been one of the core control de-
19 sign problems for applications [24, 8, 17, 15, 4]. With the rapid development of the
20 sensor technology, more and more information becomes available in advance, leading
21 to the great research interest on preview control. How to utilize the preview informa-
22 tion on disturbances to effectively improve the disturbance attenuation performance
23 is the problem of our concern. The H_∞ control problem for disturbance attenuation
24 with preview information has been known to be a challenging one for a long time and
25 was stated as Open Problem 51 in 1998 [3]. For deterministic systems, the problem
26 was finally solved in 2005 for the continuous-time case [26] and the discrete-time case
27 [27].

28 Other alternative solutions to the H_∞ control with disturbance preview for deter-
29 ministic systems can be found in the literature as well. For example, the H_∞ control
30 for deterministic systems with both input delay and disturbance preview was solved
31 in [19, 20]. Under the assumption that the standard H_∞ problem (which corresponds
32 to the system without input delay and preview) is solvable, an analytic solution to the
33 problem was provided by deriving the explicit expressions of some abstract operators
34 in [19, 20]. But as pointed out in [26], this assumption leads to a sufficient condition
35 only because the achievable H_∞ performance level by using disturbance preview is
36 typically lower (better) than that achievable by the standard H_∞ solution. In [29],
37 using the so-called reorganization technique, the H_∞ preview problem was solved and

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[†]School of Information Engineering, Zhejiang Institute of Technology, Hangzhou 310023, China (whx1123@126.com).

[‡]School of Electrical Engineering and Computer Science, University of Newcastle, Callaghan NSW 2308, Australia (minyue.fu@newcastle.edu.cn), School of Automation, Guangzhou University of Technology, and Guangdong Key Laboratory of Intelligent Decision and Cooperative Control, Guangzhou 510006, China.

[§]Corresponding author, School of Control Science and Engineering, Shandong University, Jinan, Shandong 250061, China (hszhang@sdu.edu.cn).

38 a duality between the H_∞ smoothing and the H_∞ control with input-delay and dis-
 39 turbance preview was established. However, there has been no progress so far for
 40 stochastic systems.

41 The purpose of this paper is to generalize the work in [26, 27] to the stochastic
 42 setting. Stochastic systems involve parameter uncertainties in the system model which
 43 are random in nature. Examples of random physical parameters include impedance
 44 variations in electrical circuits [7], stiffness, damping and inertia changes in mechanical
 45 systems [16], and and gravitational field fluctuations in satellite dynamics [25].

46 Our motivation stems from the fact that technical tools used in [26, 27] are suit-
 47 able for deterministic systems only. More precisely, [26, 27] gives a very elegant
 48 solvability condition for H_∞ control with disturbance preview and provides an an-
 49 alytic solution using two Riccati equations with the same dimension as the system
 50 without preview. This is made possible fundamentally due to the separation principle
 51 [1] for deterministic systems. Unfortunately, H_∞ control for stochastic systems with
 52 disturbance preview is inherently different from the deterministic case because the
 53 separation principle no longer holds [18, 6].

54 Several contributions are made in the paper. Firstly, the necessary condition of
 55 the H_∞ control for stochastic systems with preview disturbance is presented by a
 56 pair of variables admitting a forward-backward stochastic system and two stationary
 57 equations. The condition is a counterpart for bi-objective problem of the maximum
 58 principle for stochastic systems. Secondly, the affine link between the states of the
 59 forward-backward system is established. More precisely, the link is between the full-
 60 information (state and the disturbance preview) and the state of the backward system.
 61 Thirdly, an inertia condition which is necessary and sufficient for the solvability of
 62 H_∞ control problem for stochastic systems is provided. Fourthly, an analytic solution
 63 to the H_∞ preview control for stochastic systems is given.

64 Our results above are novel because the existing results [12, 13, 22, 21, 23] are
 65 for the H_∞ tracking for stochastic systems with reference signal preview. They are
 66 extensions of the work [5] rather than [27]. When the preview is on reference signal
 67 instead of disturbance in [12, 13, 22, 21, 23], as [26] pointed out, the preview informa-
 68 tion is treated in the H_2 setting rather than the H_∞ setting. In our case, the problem
 69 of H_∞ control with disturbance preview is much more involved than the H_∞ tracking
 70 problem with reference signal preview [12, 13, 22, 21, 23]. Technically speaking, our
 71 problem leads to a totally different solvability condition.

72 The rest of this paper is organized as follows. The problem to be solved is formu-
 73 lated in Section 2. A necessary condition for the solving H_∞ control with disturbance
 74 preview is presented in Section 3. The necessary condition is proved to be sufficient in
 75 Section 4. Some further discussion concerning how to use the disturbance preview to
 76 improve the closed-loop system performance is given in Section 5. Section 6 provides
 77 a quarter vehicle active suspension system to illustrate the application of our control
 78 law. Some concluding remarks are given in Section 7.

79 Notations: In the paper, w_k is a white noise with zero mean and variance σ , and
 80 it is defined on a complete probability measurable space (Ω, \mathcal{F}, P) ; \mathcal{F}_k represents a
 81 σ -algebra generated by $\{w_i, i = 0, \dots, k\}$; $E[X]$ is the expectation of the random
 82 variable X ; $E[X|\mathcal{F}]$ is the conditional expectation of the random variable X given
 83 σ -algebra \mathcal{F} ; l_2 is a space of expectation-square-summable and adapted sequences,
 84 i.e. for any $x \in l_2$, $\sum_{i=0}^{\infty} E[x'_i x_i] < \infty$ and x_i is \mathcal{F}_{i-1} -measurable. $l_{2[a,b]}$ means that
 85 every sequence here is defined over the interval $[a, b]$ [2]; For any $x, y \in l_{2[a,b]}$, $\langle x, y \rangle =$
 86 $\sum_{i=a}^b E[x'_i y_i]$ and $(l_{2[a,b]}, \langle \cdot, \cdot \rangle)$ is also a Hilbert space. If $i > j$, then $\sum_i^j a_k = 0$. For

87 any integer n and $m = 1, \dots, d$, $n_m = n + d - m$. For any matrix M , $M > 0$ ($M \geq 0$)
 88 means that M is positive definite (semi-definite).

89 **2. Problem statement.** The system to be considered in this paper is

90 (2.1)
$$x_{k+1} = A_k x_k + B_k u_k + C_k v_{k-d}$$

91 (2.2)
$$z_k = F_k x_k + D_k u_k$$

92 where x_k, u_k, z_k are state, control input, and the output to be regulated, and v_k
 93 is energy-bounded previewed exogenous disturbance with preview length $d > 0$, a
 94 integer; $A_k = A + w_k \bar{A}, B_k = B + w_k \bar{B}, C_k = C + w_k \bar{C}, F_k = F + w_k \bar{F}, D_k =$
 95 $D + w_k \bar{D}$; w_k is a scalar random white noise with zero mean and variance σ^2 and
 96 $A, \bar{A}, B, \bar{B}, C, \bar{C}, D, \bar{D}, F$ and \bar{F} are constant matrices with compatible dimensions.

97 In fact, it is shown that a large class of linear systems have their matrices
 98 A_k, B_k, C_k, D_k, F_k depending linearly on physical parameters [4]. When a physical
 99 parameter deviates from its nominal value due to various stochastic disturbances
 100 (e.g., thermal noises, vibration, impedance variations, etc.), it can be modeled as the
 101 nominal value plus some random noise. This will result in the multiplicative noise
 102 model considered in this paper.

103 Throughout the rest of this paper, we adopt the following assumption:

104 (2.3)
$$\bar{F} = 0, \bar{D} = 0, D'[D \ F] = [I \ 0]$$

105 which means that $E[z'_k z_k] = E[x'_k F' F x_k] + E[u'_k u_k]$. This will considerably reduce the
 106 complexity of required algebraic manipulations in the derivation of our some results
 107 and our idea is actually applicable to the general case without this assumption.

108 In the preview control setting, both the disturbance v_k and the control u_k are
 109 \mathcal{F}_{k-1} -adapted. Because v_k is available at time k but delayed, i.e., v_{k-d} is applied
 110 to the system at time k , u_k (being \mathcal{F}_{k-1} -adapted) would have the full information
 111 of a window of the “future” disturbance values $v_{k-d}, v_{k-d+1}, \dots, v_k$. This future in-
 112 formation makes the preview control particularly interesting in applications where
 113 adversaries (i.e. disturbances) have sluggish reactions which can be effectively mod-
 114 elled by time delays. However, how to utilize the future information to achieve the
 115 better control performance also makes the control problem technically challenging at
 116 the same time.

117 Given a control law u_k , the l_2 induced norm of the closed-loop mapping $L_{vz} :$
 118 $v \rightarrow z$ of (2.1)-(2.2) subject to the zero initial condition, i.e., $x_0 = 0, v_s = 0$ for
 119 $s = -d, \dots, -1$, is given by

120 (2.4)
$$\|L_{vz}\| = \sup_{v \in l_2} \frac{\|z\|_{l_2[0, N]}}{\|v\|_{l_2[0, N-d]}}$$

121 System (2.1)-(2.2) is said to satisfy a given H_∞ performance level $\gamma > 0$ if the
 122 following holds:

123 (2.5)
$$\|L_{vz}\| < \gamma$$

124 The H_∞ preview control problem in this paper is to testify for a given $\gamma > 0$,
 125 whether there exists a full-information and adapted control law satisfying the H_∞
 126 performance (2.5) and if exists, provides such a control law.

127 *Remark 2.1.* Adaptedness is one of the most significant differences between the
 128 deterministic and stochastic systems. Every variable appearing in the controlled sto-
 129 chastic system is required to be adapted. It also leads to the essential difference

130 between backward stochastic systems and backward deterministic systems. Unlike
 131 the case of backward deterministic systems, it is very difficult to get an explicit and
 132 analytic solution for a delayed backward stochastic system.

133 **3. Necessary condition of H_∞ control for stochastic systems with pre-**
 134 **view.** In this section, we will see what happens when there is a full-information and
 135 adapted controller such that the H_∞ performance (2.5) holds for the given γ , which
 136 in turn will be helpful for us to find a criteria to testify if there exists such a controller
 137 such that (2.5) holds for a given γ in the next section.

138 Define

$$139 \quad (3.1) \quad J(0, N) = \|z\|_{l_2[0, N]}^2 - \gamma^2 \|v\|_{l_2[0, N-d]}^2$$

140 There is a relationship between the H_∞ control performance (2.5) and dynamic
 141 game

$$142 \quad (3.2) \quad \max_v \min_u J(0, N)$$

143 because

$$144 \quad (3.3) \quad \inf_u \sup_{v \in l_2} \frac{\|z\|_{l_2[0, N]}}{\|v\|_{l_2[0, N-d]}} \leq \sup_{v \in l_2} \inf_u \frac{\|z\|_{l_2[0, N]}}{\|v\|_{l_2[0, N-d]}}$$

145 Obviously, the upper value (the left of (3.3)) is not less than the lower value (the
 146 right of (3.3)) [2]. Hence, for a given $\gamma > 0$, if $\inf_u \sup_{v \in l_2} \frac{\|z\|_{l_2[0, N]}}{\|v\|_{l_2[0, N-d]}} < \gamma$, then

147 $\sup_{v \in l_2} \inf_u \frac{\|z\|_{l_2[0, N]}}{\|v\|_{l_2[0, N-d]}} < \gamma$, and the latter can be converted into the solvable mini-
 148 max problem (3.2). Moreover, the optimal u_k, v_k admit the identical equations with
 149 the H_∞ central controller (please refer to Chapter 9 of [14]) and the worst-case distur-
 150 bance. Based on this, we propose a necessary condition for the solvable H_∞ preview
 151 control problem.

152 **LEMMA 3.1.** *Consider the system (2.1)-(2.2). If there exists a adapted controller*
 153 *such that (2.5) holds, then for $k \geq 0$, the H_∞ central controller and the worst-case*
 154 *disturbance obey the following relations*

$$155 \quad (3.4) \quad 0 = E[B'_k \lambda_k | \mathcal{F}_{k-1}] + u_k$$

$$156 \quad (3.5) \quad 0 = E[C'_{k+d} \lambda_{k+d} | \mathcal{F}_{k-1}] - \gamma^2 v_k$$

157 where

$$158 \quad (3.6) \quad \lambda_{k-1} = E[A'_k \lambda_k | \mathcal{F}_{k-1}] + F' F x_k$$

$$159 \quad (3.7) \quad \lambda_N = 0$$

160 Lemma 3.1 will be proved with the aid of projection principle in Krein space [26].
 161 It is stated as follows.

162 **LEMMA 3.2.** *Let \mathcal{X} and \mathcal{Y} be Hilbert spaces with bounded linear operators $J : \mathcal{X} \rightarrow$*
 163 *\mathcal{Y} and $S : \mathcal{X} \rightarrow \mathcal{Y}$. Suppose $J = J'$ and $S'JS > \epsilon I$ for some $\epsilon > 0$. Then, given any*
 164 *$y \in \mathcal{Y}$, there exists a unique solution to the optimization problem*

$$165 \quad (3.8) \quad \min_{x \in \mathcal{X}} \|Sx - y\|_J^2 = \min_{x \in \mathcal{X}} \langle (Sx - y), J(Sx - y) \rangle$$

166 *This solution is defined by y and a bounded linear operator, $x^* = (S'JS)^{-1}S'y$.*
 167 *Equivalently, x^* is completely characterized by the equality $S'J(Sx^* - y) = 0$, i.e.,*
 168 *$\forall x \in \mathcal{X}, \langle Sx, J(Sx^* - y) \rangle = 0$.*

169 Now we are in the position to prove Lemma 3.1.

170 *Proof.* As mentioned earlier, if the H_∞ preview control for (2.1)-(2.2) is solvable,
171 the game problem (3.2) is solvable.

172 From (3.1),

$$\begin{aligned}
 173 \quad J(0, N) &= E\left[\sum_{k=0}^N z'_k z_k - \gamma^2 \sum_{k=0}^{N-d} v'_k v_k\right] \\
 174 \quad (3.9) \quad &= E\left[\sum_{k=0}^N x'_k F' F x_k + u'_k u_k - \gamma^2 \sum_{k=0}^{N-d} v'_k v_k\right]
 \end{aligned}$$

175 Firstly, we consider the inner optimization $\min_u \|z\|_{l_2[0, N]}^2$ of (3.2). Denote the
176 input-output operators from the inputs u, v and initial data (x_0, \hat{v}_0) to the output as
177 $\mathcal{T}_u, \mathcal{T}_v$ and \mathcal{T}_0 , respectively. According to Lemma 3.2, \mathcal{T}_u , the identity operator and
178 $\mathcal{T}_v v + \mathcal{T}_0(x_0, \hat{v}_0)$ will play the roles of S, J and $-y$, respectively. The fact $\|\mathcal{T}_u u\|_{l_2[0, N]}^2 >$
179 0 for $u \neq 0$ means $S'JS = S'S$ is uniform positive. Hence, a unique optimal u ,
180 denoted by u^* minimizing $\|z\|_{l_2[0, N]}^2$ obeys

$$181 \quad (3.10) \quad \langle \mathcal{T}_u u, \mathcal{T}_u u^* + \mathcal{T}_v v + \mathcal{T}_0(x_0, \hat{v}_0) \rangle = 0$$

182 The above means that the optimal z is orthogonal to the output of any input u , which
183 is also very useful for finding the optimal solution to the outer optimization. Denoting
184 z^* as the optimal z corresponding any given v and initial data (x_0, \hat{v}_0) , (3.10) can be
185 rewritten as

$$186 \quad (3.11) \quad \langle u, \mathcal{T}'_u z^* \rangle = 0$$

187 In order to obtain the relation (3.4), the adjoint operator \mathcal{T}'_u of the operator \mathcal{T}_u
188 is characterized in the sequel.

189 Straightforward calculation shows that the k^{th} component of $\mathcal{T}_u u$ is as

$$190 \quad (3.12) \quad (\mathcal{T}_u u)_k = F \sum_{i=0}^{k-2} F(k-2, i+1) B_i u_i + D u_{k-1}$$

$$191 \quad (3.13) \quad \mathcal{T}_u u = \begin{bmatrix} D u_0 \\ F \sum_{i=0}^0 F(0, i+1) B_i u_i + D u_1 \\ \vdots \\ F \sum_{i=0}^{k-1} F(k-1, i+1) B_i u_i + D u_k \\ \vdots \end{bmatrix}$$

192 where

$$193 \quad (3.14) \quad F(k, i) = \begin{cases} A_k A_{k-1} \cdots A_i, & k \geq i \\ I, & k = i - 1 \\ 0, & k < i - 1 \end{cases}$$

194 Similarly, we can give the k^{th} components of $\mathcal{T}_v v$ and $\mathcal{T}_0(x_0, \hat{v}_0)$ as follows

$$195 \quad (3.15) \quad (\mathcal{T}_v v)_k = F \sum_{i=d}^{k-2} F(k-2, i+1) C_i v_{i-d}$$

$$196 \quad (3.16) \quad (\mathcal{T}_0(x_0, \hat{v}_0))_k = F F(k-2, 0) x_0 + F \sum_{i=0}^{\min\{k-2, d-1\}} F(k-2, i+1) C_i v_{i-d}$$

197 Hence,

$$198 \quad (3.17) \quad \mathcal{T}_u = \begin{bmatrix} D & 0 & \cdots & 0 \\ F(0,1)B_0 & D & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ F(N-1,1)B_0 & F(N-1,2)B_1 & \cdots & D \end{bmatrix}$$

199 Denote the optimal state and output generated by the optimal control law u_k^* as x_k^*
200 and z_k^* , respectively. The adaptedness of $\mathcal{T}'_u z^*$ and (3.17) together with the equality

$$201 \quad (3.18) \quad \langle \mathcal{T}_u u, z^* \rangle = \langle u, \mathcal{T}'_u z^* \rangle$$

202 show the k^{th} component of $\mathcal{T}'_u z^*$

$$203 \quad (3.19) \quad (\mathcal{T}'_u z^*)_k = D' z_{k-1}^* + E[B'_{k-1} \sum_{i=k}^N F(i-1, k)' F' z_i^* | \mathcal{F}_{k-2}]$$

204 In virtue of the assumption (2.3), the above relation can be reduced to

$$205 \quad (3.20) \quad (\mathcal{T}'_u z^*)_k = u_{k-1}^* + E[B'_{k-1} \sum_{i=k}^N F(i-1, k)' F' F x_i^* | \mathcal{F}_{k-2}]$$

206 Let

$$207 \quad (3.21) \quad \lambda_{k-1}^* = E[A'_k \lambda_k | \mathcal{F}_{k-1}] + F' F x_k$$

$$208 \quad (3.22) \quad \lambda_N^* = 0.$$

209 Then (3.20) can be rewritten as

$$210 \quad (3.23) \quad (\mathcal{T}'_u z^*)_k = u_{k-1}^* + E[B'_{k-1} \lambda_{k-1}^* | \mathcal{F}_{k-2}]$$

211 which together with (3.11) shows that the optimal u_{k-1}^* admits

$$212 \quad (3.24) \quad 0 = u_{k-1}^* + E[B'_{k-1} \lambda_{k-1}^* | \mathcal{F}_{k-2}]$$

213 Hence, (3.4) holds. Note, in particular, that u_k is \mathcal{F}_{k-1} adapted.

214 Next we consider the outer optimization problem in (3.2) over v_k . Since the H_∞
215 control problem is solvable, the inequality (2.5) subject to a admissible and adapted
216 control law u_k^* holds for any disturbance v_k and zero initial state, namely,

$$217 \quad (3.25) \quad \sup_{v \in \mathcal{L}_2} \frac{\|z^*\|_{\mathcal{L}_2[0, N]}^2}{\|v\|_{\mathcal{L}_2[0, N-d]}^2} < \gamma^2$$

218 Therefore,

$$219 \quad (3.26) \quad \gamma^2 \|v\|_{\mathcal{L}_2[0, N-d]}^2 - \|z^*\|_{\mathcal{L}_2[0, N-d]}^2 > 0$$

220 Denoting $J = \text{diag}\{\gamma^2 I, -I\}$ and $Sv = (v, \mathcal{T}_v v + \mathcal{T}_u u^*)$, the inequality (3.26)
221 implies $S'JS$ is a positive operator.

222 We now solve the outer optimization in (3.2) according to Lemma 3.2. Let
223 $(0, \mathcal{T}_0(x_0, \hat{v}_0))$ and v play the roles of $-y$ and x in Lemma 3.2, then $J^*(0, N)$ in
224 (3.2) can be rewritten as

$$225 \quad (3.27) \quad J^*(0, N) = \langle Sv + (0, \mathcal{T}_0 x_0), J[Sv + (0, \mathcal{T}_0 x_0)] \rangle$$

226 where $J^*(0, N)$ means the J driven by u^* . The positive definiteness of $S'JS$ implies
 227 that $\max_v J^*(0, N)$ is solvable and the optimal v solving $\max_v J^*(0, N)$, denoted as
 228 $v^\#$, satisfying the relation below

229 (3.28)
$$S'J[Sv^\# + (0, \mathcal{T}_0x_0)] = 0$$

230 i.e.

231 (3.29)
$$S'J(v^\#, z^\#) = 0$$

232 where $z^\#$ is the output driven by the optimal u^* , the optimal $v^\#$ and the any given
 233 initial data (x_0, \hat{v}_0) . Different from the inner optimization in (3.2), it is not easy to
 234 derive the adjoint operator S' from the equation (3.29) to characterize the optimal
 235 $v^\#$. We thus introduce a new operator \tilde{S} as

236 (3.30)
$$\tilde{S}v = (v, \mathcal{T}_v v)$$

237 Here note that, as a candidate of z^* , $z^\#$ is generated by the optimal control u^* , the
 238 optimal v^* and any given initial data (x_0, \hat{v}_0) , which together with (3.10) shows $z^\#$ is
 239 orthogonal to the output $\mathcal{T}_u u$ for any u , one of which is $\mathcal{T}_u u^*$. Hence, $\langle z^\#, \mathcal{T}_u u^* \rangle = 0$.
 240 Based on it, (3.29) can read as

241 (3.31)
$$\begin{aligned} 0 &= \langle Sv, J(v^\#, z^\#) \rangle \\ 242 &= \langle (v, \mathcal{T}_v v + \mathcal{T}_u u^*), J(v^\#, z^\#) \rangle \\ 243 &= \gamma^2 \langle v, v^\# \rangle - \langle \mathcal{T}_v v + \mathcal{T}_u u^*, z^\# \rangle \\ 244 &= \gamma^2 \langle v, v^\# \rangle - \langle \mathcal{T}_v v, z^\# \rangle \\ 245 &= \langle \tilde{S}v, J(v^\#, z^\#) \rangle \end{aligned}$$

246 i.e.,

247 (3.32)
$$\tilde{S}'J(v^\#, z^\#) = 0$$

248 Since $\tilde{S}'(v, z) = v + \mathcal{T}_v' z$,

249 (3.33)
$$0 = \tilde{S}'J(v^\#, z^\#) = \gamma^2 v^\# - \mathcal{T}_v' z^\#$$

250 which implies that the k^{th} component of $\mathcal{T}_v' z^\#$ equals to

251 (3.34)
$$\begin{aligned} (\mathcal{T}_v' z^\#)_k &= E[C'_{k-1} \sum_{i=k}^N F(i-1, k)' F' z_i^\# | \mathcal{F}_{k-2}]' \\ 252 &= \gamma^2 v_{k-1-d}^\# \end{aligned}$$

253 Let

254 (3.35)
$$\lambda_{k-1}^\# = E[A'_k \lambda_k^\# | \mathcal{F}_{k-1}] + F' F x_k^\#$$

255 (3.36)
$$\lambda_N^\# = 0.$$

256 the equation (3.34) can be reduced to

257 (3.37)
$$E[C'_{k-1} \lambda_{k-1}^\# | \mathcal{F}_{k-2-d}]' = \gamma^2 v_{k-1-d}^\#$$

258 In the above, all the variables labeled by $\#$ have a similar meaning as $z^\#$ and are
 259 optimal trajectories corresponding to the optimal $v^\#$ and the optimal u^* . Here, u^*
 260 can be denoted as $u^\#$ since u_k can obtain the information of v_k and u_k^* actually
 261 depends on $v^\#$ when v_k equals to $v^\#$.

262 At present, all the variables $x_k, u_k, v_k, z_k, \lambda_k$ are unified and labeled by $\#$. For
 263 notational simplicity, we omit the superscript $\#$ in (3.35)-(3.36), we get (3.6)-(3.7),
 264 which means that the optimal u and v can be characterized by the unified (3.6)-(3.7).
 265 The conclusion in this lemma is thus proved. \square

266 *Remark 3.3.* Lemma 3.1 proposes a necessary condition of the solvable minimax
 267 problem (3.2) by the projection principle in indefinite space, which is very helpful for
 268 characterizing the optimal trajectories of (3.2) by a unified pair of variables and thus
 269 pursuing the optimal solution to the minimax problem (3.2).

270 *Remark 3.4.* Lemma 3.1 is an analogue for the minimax problem of the maximum
 271 principle for the optimal problem [28].

272 Lemma 3.1 implicitly describes a necessary condition, in the form of equations
 273 satisfied by the H_∞ preview controller and the worst-case disturbance, of the solvable
 274 H_∞ preview control problem, and what follows is an explicit expression.

275 **LEMMA 3.5.** *Consider the system (2.1)-(2.2). If there exists a adapted controller*
 276 *such that (2.5) holds, then*

- 277 • R_k and Λ have the same inertias, i.e. the numbers of negative, positive and
- 278 zero eigenvalues of R_k and Λ are equal, respectively;
- 279 • The H_∞ central controller u_k and the worst-disturbance v_k admit

$$280 \quad (3.38) \quad \begin{bmatrix} u_k \\ v_k \end{bmatrix} = -R_k^{-1} [T_k x_k + \sum_{j=0}^{d-1} T_k^j v_{k+j-d}]$$

- 281 • There holds

$$282 \quad (3.39) \quad \lambda_{k-1} = P_k x_k + \sum_{j=0}^{d-1} P_k^j v_{k+j-d}$$

283

$$284 \quad (3.40) \quad \lambda_{k+d-1} = S_k x_k + \sum_{j=0}^{d-1} S_k^j v_{k+j-d}$$

285 In the above,

$$286 \quad (3.41) \quad \Lambda = \text{diag}\{I, -\gamma^2 I\}$$

287

$$288 \quad (3.42) \quad R_k = E \begin{bmatrix} B'_k P_{k+1} B_k & B'_k P_{k+1}^{d-1} \\ C'_{k+d} S_{k+1} B_k & C'_{k+d} S_{k+1}^{d-1} \end{bmatrix} + \Lambda$$

289 and P_k, P_k^j admit the following recursive relations

$$290 \quad (3.43) \quad P_k = E[A'_k P_{k+1} A_k] + F' F - \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ (P_{k+1}^{d-1})' A \end{bmatrix}' R_k^{-1} T_k$$

$$291 \quad (3.44) \quad P_k^0 = E[A'_k P_{k+1} C_k] - \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ (P_{k+1}^{d-1})' A \end{bmatrix}' R_k^{-1} T_k^0$$

$$292 \quad (3.45) \quad P_k^j = A' P_{k+1}^{j-1} - \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ (P_{k+1}^{d-1})' A \end{bmatrix}' R_k^{-1} T_k^j$$

293 with

$$294 \quad (3.46) \quad T_k = \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ E[C'_{k+d} S_{k+1}] A \end{bmatrix}$$

$$295 \quad (3.47) \quad T_k^0 = \begin{bmatrix} E[B'_k P_{k+1} C_k] \\ E[C'_{k+d} S_{k+1}] C \end{bmatrix}$$

$$296 \quad (3.48) \quad T_k^j = \begin{bmatrix} B' P_{k+1}^{j-1} \\ E[C'_{k+d} S_{k+1}^{j-1}] \end{bmatrix}, j = 1, \dots, d-1$$

297 Therein, $P_{N+1}^j = 0$, S_k and S_k^j , which are initialized by $S_{N+1} = 0$ and $S_{N+1}^j = 0$,
 298 contain the noises w_k, \dots, w_{k+d-1} will be explicitly given in the next lemma.

299 *Proof.* The proof is stated in Appendix. □

300 Until now S_{k+1} and $S_{k+1}^j, j = 0, \dots, d-1$ involved in Lemma 3.5 still remain to
 301 be given. To the end, it is necessary to define some notations.

$$302 \quad (3.49) \quad \Phi_n^{k+1} = \Phi_{n+k}^1 \Phi_n^k + \sum_{f=0}^{k-1} \Phi_{n+k}^{1,f+d-k} \Pi_n^f$$

$$303 \quad \Phi_n^{k+1,j} = \Phi_{n+k}^1 \Phi_n^{k,j} + \sum_{f=0}^{k-1} \Phi_{n+k}^{1,f+d-k} \Pi_n^{f,j} + \Phi_{n+k}^{1,j-k}$$

304 (3.50)

$$305 \quad (3.51) \quad \Pi_n^k = \Pi_{n+k}^0 \Phi_n^k + \sum_{f=0}^{k-1} \Pi_{n+k}^{0,f+d-k} \Pi_n^f$$

$$306 \quad \Pi_n^{k,j} = \Pi_{n+k}^0 \Phi_n^{k,j} + \sum_{f=0}^{k-1} \Pi_{n+k}^{1,f+d-k} \Pi_n^{f,j} + \Pi_{n+k}^{0,j-k}$$

307 (3.52)

308 with the initial values

$$309 \quad (3.53) \quad \Phi_n^0 = I, \Phi_n^{0,j} = 0$$

$$310 \quad (3.54) \quad \Phi_n^1 = A_n - [B_n \ 0] R_n^{-1} T_n$$

$$311 \quad (3.55) \quad \Phi_n^{1,j} = \delta_j C_n - [B_n \ 0] R_n^{-1} T_n^j$$

$$312 \quad (3.56) \quad \Pi_n^0 = -[0 \ I] R_n^{-1} T_n,$$

$$313 \quad (3.57) \quad \Pi_n^{0,j} = -[0 \ I] R_n^{-1} T_n^j$$

314 where R_n, T_n and $T_n^j, j = 0, \dots, d-1$ are as in (3.42), (3.46)-(3.48), respectively. It
 315 should be pointed that we also need the notations $\Phi_n^j = 0$, $\Phi_n^{1,j} = 0$ and $\Pi_n^j = 0$ for
 316 $j < 0$.

317 With those notations above, the expressions of S_n and $S_n^j, j = 0, \dots, d-1$ are
 318 provided below.

319 LEMMA 3.6. The coefficient matrices S_n and S_n^j appearing in the relation (3.40)

320 with $k = n$ are given as

$$321 \quad (3.58) \quad S_n = P_{n+d} \Phi_n^d + \sum_{f=0}^{d-1} P_{n+d}^f \Pi_n^f$$

$$322 \quad (3.59) \quad S_n^j = P_{n+d} \Phi_n^{d,j} + \sum_{f=0}^{d-1} P_{n+d}^f \Pi_n^{f,j}$$

323 Moreover, S_n and $S_n^j, j = 0, \dots, d-1$ only involve noises $\{w_{n+d-1}, \dots, w_n\}$.

324 *Proof.* Let the inputs u and v be the optimal for $\max_v \min_u J(0, N)$. Then the
325 following representations can be obtained

$$326 \quad (3.60) \quad x_{n+k+1} = \Phi_n^{k+1} x_n + \sum_{j=0}^{d-1} \Phi_n^{k+1,j} v_{j+n-d}$$

$$327 \quad (3.61) \quad v_{n+k} = \Pi_n^k x_n + \sum_{j=0}^{d-1} \Pi_n^{k,j} v_{j+n-d}$$

328 by inductive derivation over $k = 0, \dots, d-1$. From these two expressions and (3.40),
329 we can get the expressions (3.58) and (3.59).

330 What follows is a brief proof for (3.60) and (3.61). According to Lemma 3.5, the
331 optimal u_n, v_n for $\max_v \min_u J(0, N)$ is

$$332 \quad (3.62) \quad u_n = -[I \ 0] R_n^{-1} (T_n x_n + \sum_{j=0}^{d-1} T_n^j v_{n+j-d})$$

$$333 \quad (3.63) \quad v_n = -[0 \ I] R_n^{-1} (T_n x_n + \sum_{j=0}^{d-1} T_n^j v_{n+j-d})$$

334 Observing (3.57), it is direct to find that the optimal v_n as in (3.63) is exactly
335 (3.61) with $k = 0$. Substituting (3.62) into (2.1), there holds

$$336 \quad (3.64) \quad x_{n+1} = \Phi_n^1 x_n + \sum_{j=0}^{d-1} \Phi_n^{1,j} v_{n+j-d}$$

337 which is (3.60) with $k = 0$.

338 Assuming (3.60) and (3.61) hold for $k = 0, \dots, s-1$ and $s < d-1$, we will verify
339 that (3.60) and (3.61) also hold for $k = s$.

340 Similar to (3.62) and (3.64), we have

$$341 \quad (3.65) \quad v_{n+s} = -[0 \ I] R_{k+s}^{-1} (T_{n+s} x_{n+s} + \sum_{j=0}^{d-1} T_{n+s}^j v_{n+s+j-d})$$

$$342 \quad (3.66) \quad x_{n+s+1} = \Phi_{n+s}^1 x_{n+s} + \sum_{j=0}^{d-1} \Phi_{n+s}^{1,j} v_{n+s+j-d}$$

343 It is easy to know that the subscript of $v_{n+s+j-d}$, namely, $n+s+j-d$ is less than
344 $n+s$ in the second term in the right side of (3.65)-(3.66) because of $j = 0, \dots, d-1$,

345 which means that $v_{n+s+j-d}$ with $s+j-d > 0$ can be re-expressed by the inductive
 346 assumption.

347 Applying the inductive assumption (3.60) with $k = s - 1$ and (3.61) with $k =$
 348 $0, \dots, s - 1$ into (3.65)-(3.66) and using the notations (3.49)-(3.52), (3.60)-(3.61) with
 349 $k = s$ are obtained.

350 Reminding of the relation (A.22), we have

$$351 \quad (3.67) \quad \lambda_{n+d-1} = P_{n+d}x_{n+d} + \sum_{j=0}^{d-1} P_{n+d}^j v_{n+j}$$

352 From (3.60)-(3.61),

$$353 \quad (3.68) \quad x_{n+d} = \Phi_n^d x_n + \sum_{j=0}^{d-1} \Phi_n^{d,j} v_{n+j-d}$$

$$354 \quad (3.69) \quad v_{n+j} = \Pi_n^j x_n + \sum_{i=0}^{d-1} \Pi_n^{j,i} v_{n+i-d}$$

355 Inserting both of them into (3.67), one will get (3.58)-(3.59). In terms of the recur-
 356 sive relations (3.49)-(3.52), we can see that $\Phi_n^d, \Phi_n^{d,j}$ and $\Pi_n^f, \Pi_n^{f,j}$ $f = 0, \dots, d - 1$
 357 only include the noises $\{w_{k+d-1}, \dots, w_n\}$ and $\{w_{k+f}, \dots, w_n\}$, respectively. As a
 358 consequence, S_n and $S_n^j, j = 0, \dots, d - 1$ only involve the noises $\{w_{n+d-1}, \dots, w_n\}$. \square

359 Lemma 3.6 shows that there are links between $P_{k+1}, P_{k+1}^j, j = 0, \dots, d - 1$ and
 360 $S_{k+1}, S_{k+1}^j, j = 0, \dots, d - 1$. The links will help us to get explicit expressions of
 361 $E[C'_{k+d}S_{k+1}]$ and $E[C'_{k+d}S_{k+1}^j], j = 0, \dots, d - 1$ appearing in (3.42), (3.46)-(3.48) in
 362 Lemma 3.5.

363 LEMMA 3.7. *The following relations hold for $k = 0, \dots, N$ and $j = 1, \dots, d$:*

$$364 \quad (3.70) \quad E[C'_{k+d}S_{k+1}] = (P_{k+1}^{d-1})'$$

$$365 \quad (3.71) \quad E[C'_{k+d}S_{k+1}^j] = m_k^j + \delta_{d-j}(C'P_{k_1}C + \sigma\bar{C}'P_{k_1}\bar{C})$$

366 with

$$367 \quad (3.72) \quad m_k^j = - \sum_{i=1}^j (T_{k+i}^{d-i})' R_{k+i}^{-1} T_{k+i}^{j-i} + \sum_{i=1}^{d-1} \delta_{i-j} (P_{k+1+i}^{d-i-1})' C$$

$$368 \quad (3.73) \quad k_1 = k + d - 1$$

369 where δ_i is a Kronecker operator with the center in 0.

370 *Proof.* The proof of Lemma 3.7 is based on Lemma 3.6 and inductive derivation
 371 over $k = N, \dots, 0$.

372 As $k = N$, (3.70) and (3.71) are trivial since the initial matrices value $S_{N+1} = 0$
 373 and $P_{N+1}^j = 0, S_{N+1}^j = 0$ with $j = 0, \dots, d - 1$.

374 Assume (3.70) and (3.71) hold for all $k \geq n$. Then (3.42), (3.46)-(3.48) can be

375 rewritten as

$$376 \quad (3.74) \quad R_k = \begin{bmatrix} E[B'_k P_{k+1} B_k] & B' P_{k+1}^{d-1} \\ (P_{k+1}^{d-1})' B & m_k^{d-1} + E[C'_k P_{k+1} C_k] \end{bmatrix} + \Lambda$$

$$377 \quad (3.75) \quad T_k = \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ E[C'_{k+d} S_{k+1}] A \end{bmatrix}$$

$$378 \quad (3.76) \quad T_k^0 = \begin{bmatrix} E[B'_k P_{k+1} C_k] \\ E[C'_{k+d} S_{k+1}] C \end{bmatrix}$$

$$379 \quad (3.77) \quad T_k^j = \begin{bmatrix} B' P_{k+1}^{j-1} \\ E[C'_{k+d} S_{k+1}^{j-1}] \end{bmatrix}, j = 1, \dots, d-1$$

380 Consequently, (3.43)-(3.45) can be reformulated as

$$381 \quad (3.78) \quad P_k = A' P_{k+1} A + \sigma \bar{A}' P_{k+1} \bar{A} - T'_k R_k^{-1} T_k + F' F$$

$$382 \quad (3.79) \quad P_k^0 = A' P_{k+1} B + \sigma \bar{A}' P_{k+1} \bar{B} - T'_k R_k^{-1} T_k^0$$

$$383 \quad (3.80) \quad P_k^j = A' P_{k+1}^{j-1} - T'_k R_k^{-1} T_k^j$$

385 What follows is to prove (3.70)-(3.71) also hold in the case of $k = n-1$.

386 These two equalities

$$387 \quad (3.81) \quad E[C'_{n_1} S_n] = (P_{n_m}^{m-1}) E[\Phi_{n_m}^{d-m}] + \sum_{f=0}^{d-1-m} [C' P_{n+d}^f$$

$$388 \quad - \sum_{i=1}^m (T_{n_i}^{i-1})' R_{n_i}^{-1} T_{n_i}^{f+i}] E[\Pi_n^f]$$

$$389 \quad (3.82) \quad E[C'_{n_1} S_n^j] = (P_{n_m}^{m-1}) E[\Phi_{n_m}^{d-m,j}] + \sum_{f=0}^{d-1-m} [C' P_{n+d}^f$$

$$390 \quad - \sum_{i=1}^m (T_{n_i}^{i-1})' R_{n_i}^{-1} T_{n_i}^{f+i}] E[\Pi_n^{f,j}]$$

$$391 \quad - \sum_{i=d-m}^j (T_{n+i}^{d-i-1})' R_{n+i}^{-1} T_{n+i}^{j-i} + \sum_{i=d-m}^{d-2} \delta_{j-i} (P_{n+i+1}^{d-i-2})' C$$

$$392 \quad + \delta_{d-1-j} E[C'_n P_{n+d} C_n]$$

393 are very useful for our proof. They can be proved by inductive derivation over $m =$
 394 $1 \dots, d$ and straightforward expectation calculation based on Lemma 3.6 and matrices
 395 (3.49)-(3.57), so we omit it here.

396 Let $m = d$ in (3.81) and (3.82), we will see (3.70) and (3.71) hold for $k = n-1$.
 397 Now the proof is completed. \square

398 According to Lemma 3.7, some matrices appearing in Lemma 3.5 are simplified
 399 further in the following remark.

400 *Remark 3.8.* Those notations related to $E[C'_{k+d} S_{k+1}]$ as well as $E[C'_{k+d} S_{k+1}^j]$,

401 appearing in Lemma 3.5 can be rewritten as

$$402 \quad (3.83) \quad T_k = \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ (P_{k+1}^{d-1})' A \end{bmatrix}$$

$$403 \quad (3.84) \quad T_k^0 = \begin{bmatrix} E[B'_k P_{k+1} C_k] \\ (P_{k+1}^{d-1})' C \end{bmatrix}$$

$$404 \quad (3.85) \quad T_k^j = \begin{bmatrix} B' P_{k+1}^{j-1} \\ (P_{k+j+1}^{d-j-1})' C - \sum_{f=1}^j (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{j-f} \end{bmatrix}$$

$$406 \quad (3.86) \quad R_k = \begin{bmatrix} E[B'_k P_{k+1} B_k] & (P_{k+1}^{d-1})' B \\ B' P_{k+1}^{d-1} & E[C'_{k+d} P'_{k+d+1} C_{k+d}] \end{bmatrix} \\ + \text{diag}\{I, -\gamma^2 I - \sum_{f=1}^d (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{d-f}\}$$

408 Further, (3.43)-(3.45) are expressed as

$$409 \quad (3.87) \quad P_k = A' P_{k+1} A + \sigma \bar{A}' P_{k+1} \bar{A} - T'_k R_k^{-1} T_k + F' F$$

$$410 \quad (3.88) \quad P_k^0 = A' P_{k+1} C + \sigma \bar{A}' P_{k+1} \bar{C} - T'_k R_k^{-1} T_k^0$$

$$411 \quad (3.89) \quad P_k^j = A' P_{k+1}^{j-1} - T'_k R_k^{-1} T_k^j$$

412 Remark 3.8 provides a more direct but equivalent result than that in Lemma 3.5,
413 which is very useful in the next section.

414 **4. Sufficient condition of H_∞ control for stochastic systems with pre-**
415 **view.** In the section, we will verify that the necessary condition in Lemma 3.5 is also
416 sufficient for the solvability of the H_∞ control problem with disturbance preview.

417 Although the same notations as the last section are introduced at the beginning
418 of this section, please note that their meanings are actually different because R_k and
419 $T_k^j, j = 1, \dots, d-1$ appearing in (4.1)-(4.3) and (3.87)-(3.89) are different.

420 Before our proof begins, we need to define some notations.

$$421 \quad (4.1) \quad P_k = A' P_{k+1} A + \sigma \bar{A}' P_{k+1} \bar{A} - T'_k R_k^{-1} T_k + F' F$$

$$422 \quad (4.2) \quad P_k^0 = A' P_{k+1} C + \sigma \bar{A}' P_{k+1} \bar{C} - T'_k R_k^{-1} T_k^0$$

$$423 \quad (4.3) \quad P_k^j = A' P_{k+1}^{j-1} - T'_k R_k^{-1} T_k^j$$

$$424 \quad (4.4) \\ 425 \quad (4.5) \quad R_k = \begin{bmatrix} E[B'_k P_{k+1} B_k] & (P_{k+1}^{d-1})' B \\ B' P_{k+1}^{d-1} & \beta_{k+1}(d-1, d-1) \end{bmatrix} + \Lambda$$

$$426 \quad (4.6) \quad T_k = \begin{bmatrix} E[B'_k P_{k+1} A_k] \\ (P_{k+1}^{d-1})' A \end{bmatrix}$$

$$427 \quad (4.7) \quad T_k^0 = \begin{bmatrix} E[B'_k P_{k+1} C_k] \\ (P_{k+1}^{d-1})' C \end{bmatrix}$$

$$428 \quad (4.8) \quad T_k^j = \begin{bmatrix} B' P_{k+1}^{j-1} \\ \beta_{k+1}(d-1, j-1) \end{bmatrix}$$

429 with

$$430 \quad (4.9) \quad \beta_k(i, j) = \beta_{k+1}(i-1, j-1) - (T_k^i)' R_k^{-1} T_k^j$$

$$431 \quad (4.10) \quad \beta_k(j, i) = \beta_k(i, j)'$$

$$432 \quad (4.11) \quad \beta_k(0, j) = C' P_{k+1}^{j-1} - (T_k^0)' R_k^{-1} T_k^j$$

$$433 \quad (4.12) \quad \beta_k(0, 0) = E[C' P_{k+1} C_k] - (T_k^0)' R_k^{-1} T_k^0$$

434 For $i = 0, \dots, d-1$ and $j = 0, \dots, d-1$, the initial matrices value of P_k^j and $\beta_k(i, j)$
435 are given as $P_{N+1}^j = 0$ and $\beta_{N+1}(i, j) = 0$.

436 *Remark 4.1.* In fact, the relationships (4.2)-(4.3) together with their initial values
437 means that $P_k^j = 0$ if $k+j-d > N-d$. Similarly, $\beta_k(i, j) = 0$ if $k+\max\{i, j\}-d > N-d$
438 follows from the relation (4.9) and the initial value of $\beta_k(i, j)$.

439 Now a condition is provided to guarantee the solvability of the H_∞ preview control
440 problem for a given γ .

441 **LEMMA 4.2.** For a given $\gamma > 0$. If (4.1)-(4.3) admit solutions such that R_k and Λ
442 have the same inertias, then the H_∞ control problem (2.5) subject to (2.1) is solvable.
443 Moreover, the H_∞ central controller u_k and the worst-disturbance v_k admit

$$444 \quad (4.13) \quad \begin{bmatrix} u_k \\ v_k \end{bmatrix} = -R_k^{-1} [T_k x_k + \sum_{j=0}^{d-1} T_k^j v_{k+j-d}]$$

445 *Proof.* Define a value function by

$$446 \quad (4.14) \quad V(k, \bar{x}_k) = E[x_k' P_k x_k + 2 \sum_{j=0}^{d-1} x_k' P_k^j v_{k+j-d} + \sum_{i=0}^{d-1} \sum_{j=0}^{d-1} v_{k+j-d}' \beta_k(i, j) v_{k+i-d}]$$

447 where $\bar{x}_k = \text{col}\{x_k, v_{k-1}, \dots, v_{k-d}\}$.

448 Then we have

$$449 \quad (4.15) \quad V(k+1, \bar{x}_{k+1}) = E[x_{k+1}' P_{k+1} x_{k+1} \\ 450 \quad + 2 \sum_{j=0}^{d-1} x_{k+1}' P_{k+1}^j v_{k+1+j-d} + \sum_{i=0}^{d-1} \sum_{j=0}^{d-1} v_{k+1+i-d}' \beta_{k+1}(i, j) v_{k+1+j-d}]$$

451 Plugging (2.1) into (4.15) and Completing square over $\text{col}\{u_k, v_k\}$ will yield

$$452 \quad (4.16) \quad V(k+1, \bar{x}_{k+1}) \\ 453 \quad = E[x_k' (A_k' P_{k+1} A_k - T_k' R_k^{-1} T_k) x_k + \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}' R_k \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix} \\ 454 \quad - u_k' u_k + \gamma^2 v_k' v_k \\ 455 \quad + 2x_k' (A_k' P_{k+1} C_k - T_k' R_k^{-1} T_k^0) v_{k-d} + 2x_k' \sum_{j=1}^{d-1} (A_k' P_{k+1}^{j-1} - T_k' R_k^{-1} T_k^j) v_{k+j-d} \\ 456 \quad + v_{k-d}' C_k' P_{k+1} C_k v_{k-d} - \sum_{i=0}^{d-1} \sum_{j=0}^{d-1} v_{k+i-d}' (T_k^i)' R_k^{-1} T_k^j v_{k+j-d} \\ 457 \quad + 2 \sum_{j=1}^{d-1} v_{k-d}' C_k' P_{k+1}^{j-1} v_{k+j-d} + \sum_{i=1}^{d-1} \sum_{j=1}^{d-1} v_{k+i-d}' \beta_{k+1}(i-1, j-1) v_{k+j-d}]$$

458 where

$$459 \quad (4.17) \quad \begin{bmatrix} \bar{u}_k^* \\ \bar{v}_k^* \end{bmatrix} = R_k^{-1} (T_k x_k + \sum_{j=0}^{d-1} T_k^j v_{k+j-d})$$

460 Applying (4.1)-(4.3), (4.9) and (4.11)-(4.12) in (4.16) yields

$$461 \quad V(k+1, \bar{x}_{k+1}) \\ 462 \quad = E[x_k'(P_k - F'F)x_k + \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}' R_k \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}] \\ 463 \quad - u_k' u_k + \gamma^2 v_k' v_k \\ 464 \quad + 2x_k' \sum_{j=0}^{d-1} P_k^j v_{k+j-d} + \sum_{i=0}^{d-1} \sum_{j=0}^{d-1} v_{k+i-d}' \beta_k(i, j) v_{k+j-d}]$$

465 Now it is straightforward to obtain

$$466 \quad (4.18) \quad V(k, \bar{x}_k) - V(k+1, \bar{x}_{k+1}) \\ 467 \quad = E[x_k' F' F x_k + u_k' u_k - \gamma^2 v_k' v_k - \sum_{k=0}^N \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}' R_k \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}] \\ 468 \quad = E[z_k' z_k - \gamma^2 v_k' v_k - \sum_{k=0}^N \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}' R_k \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}]$$

469 Adding (4.18) from $k = 0$ to $k = N$, we have

$$470 \quad (4.19) \quad V(0, \bar{x}_0) - V(N+1, \bar{x}_{N+1}) \\ 471 \quad = \sum_{k=0}^N E[z_k' z_k - \gamma^2 v_k' v_k] + \sum_{k=0}^N \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}' R_k \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}$$

472 As $k = N+1$, $V(N+1, \bar{x}_{N+1}) = x_{N+1}' P_{N+1} x_{N+1}$ from (4.14) and Remark 4.1; On the
473 other hand, as $k > N-d$, $R_k = \text{diag}\{E[B_k' P_{k+1} B_k + I], -\gamma^2 I\}$ from (4.5) and Remark
474 4.1; $v_k^* = 0$ because the blocks in T_k and T_k^j , $j = 0, \dots, d-1$ corresponding to v_k are
475 null, which originates from Remark 4.1, as $k > N-d$, $P_k^{d-1} = 0$ and $\beta_k(d-1, j) = 0$.

476 Now it is easy to get from (4.19)

$$477 \quad (4.20) \quad J = V(0, \bar{x}_0) + \sum_{k=0}^N \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix}' R_k \begin{bmatrix} u_k + \bar{u}_k^* \\ v_k + \bar{v}_k^* \end{bmatrix} + \gamma^2 \sum_{k=N-d+1}^N v_k' v_k$$

478 Given that R_k and Λ have the same inertia, (4.20) shows that $J < 0$ holds when
479 the initial data $\bar{x}_0 = 0$ and $u_k = \bar{u}_k^*$. \square

480 At the moment, we associate the sufficient condition in Lemma 4.2 with the nec-
481 essary condition in Lemma 3 and give the following necessary and sufficient condition
482 for the solvability of the H_∞ preview control.

483 **THEOREM 4.3.** *For a given $\gamma > 0$, the H_∞ preview control problem (2.5) subject*
484 *to (2.1) is solvable if and only if (3.87)-(3.89) with 3.83-3.86 admit solutions such*

485 that $\text{diag}\{\Omega_k, \Delta_k\}$ and Λ have the same inertias. Moreover, the H_∞ preview control
486 law is given as

$$487 \quad (4.21) \quad u_k = -\Omega_k^{-1}(E[B'_k P_{k+1} A_k]x_k + E[B'_k P_{k+1} C_k]v_{k-d}) \\ 488 \quad \quad \quad + \sum_{j=1}^d B' P_{k+1}^{j-1} v_{k+j-d}$$

489 In the above,

$$490 \quad (4.22) \quad \Omega_k = I + B' P_{k+1} B + \sigma \bar{B}' P_{k+1} \bar{B} \\ 491 \quad (4.23) \quad \Delta_k = -\gamma^2 I + C' P_{k+d+1} C + \sigma \bar{C}' P_{k+d+1} \bar{C} \\ 492 \quad \quad \quad - \sum_{f=1}^d (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{d-f} - (P_{k+1}^{d-1})' B \Omega_k^{-1} B' P_{k+1}^{d-1}$$

493 *Proof.* The straightforward calculation shows the explicit expressions of $\beta_k(i, j)$
494 in the aforementioned as follows. In the case of $i < j$, from (4.9) and (4.11),

$$495 \quad (4.24) \quad \beta_k(i, j) = C' P_{k+i+1}^{j-i-1} - \sum_{f=0}^i (T_{k+f}^{i-f})' R_{k+f}^{-1} T_{k+f}^{j-f}$$

496 In the case of $i = j$, from (4.9) and (4.12),

$$497 \quad (4.25) \quad \beta_k(i, j) = E[C'_{k+i} P_{k+i+1} C_{k+i}] - \sum_{f=0}^i (T_{k+f}^{i-f})' R_{k+f}^{-1} T_{k+f}^{i-f}$$

498 As for the case of $i > j$, the explicit expression will be given by (4.10).

499 With the explicit expression of $\beta_k(i, j)$, R_k and $T_k^j, j = 1, \dots, d-1$ can be read
500 as

$$501 \quad (4.26) \quad T_k^j = \left[\begin{array}{c} B' P_{k+1}^{j-1} \\ (P_{k+j+1}^{d-j-1})' C - \sum_{f=1}^j (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{j-f} \end{array} \right]$$

$$502 \quad (4.27) \quad R_k = \left[\begin{array}{cc} E[B'_k P_{k+1} B_k] & (P_{k+1}^{d-1})' B \\ B' P_{k+1}^{d-1} & E[C'_{k+d} P'_{k+d+1} C_{k+d}] \end{array} \right]$$

$$503 \quad \quad \quad + \text{diag}\{I, -\gamma^2 I - \sum_{f=1}^d (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{d-f}\}$$

504 Now it is clear that (4.1)-(4.3) can be reformulated as (3.87)-(3.89), which together
505 with Lemma 3.5 and Lemma (4.2) shows H_∞ control problem is solvable if and only
506 if (3.87)-(3.89) have solutions such that R_k and Λ have the same inertia. In order to
507 obtain a preview control law, after making a LDU decomposition for R_k , (4.20) can
508 be rewritten as

$$509 \quad (4.28) \quad J(0, N) = V(0, \bar{x}_0) + \sum_{k=0}^N (u_k + \check{u}_k^*)' \Omega_k (u_k + \check{u}_k^*) \\ 510 \quad \quad \quad + \sum_{k=0}^{N-h} (v_k + \hat{v}_k^*)' \Delta_k (v_k + \hat{v}_k^*)'$$

511 with

$$512 \quad (4.29) \quad \check{u}_k^* = \Omega_k^{-1}(E[B'_k P_{k+1} A_k]x_k + E[B'_k P_{k+1} C_k]v_{k-d})$$

$$513 \quad + \sum_{j=1}^d B' P_{k+1}^{j-1} v_{k+j-d}$$

514 and $\hat{v}_k^* = \bar{v}_k^*$ as in (4.17). Consequently, the H_∞ preview control law can be chosen
 515 as $-\check{u}_k^*$, i.e., (4.21). \square

516 To compare the performances of the H_∞ preview control and the standard H_∞
 517 full-information control, we present the following theorem.

518 **THEOREM 4.4.** *For a given $\gamma > 0$, the H_∞ full-information control problem (2.5)*
 519 *subject to (2.1) with $d = 0$ is solvable if and only if*

$$520 \quad (4.30) \quad P_k = A' P_{k+1} A + \sigma \bar{A}' P_{k+1} \bar{A} - T'_k R_k^{-1} T_k + F' F$$

521 *admit solutions such that $\text{diag}\{\Omega_k, \Delta_k\}$ and $\text{diag}\{I, -\gamma^2 I\}$ have the same inertia.*
 522 *Moreover, the H_∞ full-information control law is given as*

$$523 \quad (4.31) \quad u_k = -\Omega_k^{-1}(E[B'_k P_{k+1} A_k]x_k + E[B'_k P_{k+1} C_k]v_k)$$

524 *In the above,*

$$525 \quad (4.32) \quad R_k = \begin{bmatrix} E[B'_k P_{k+1} B_k] + I & E[B'_k P_{k+1} C_k] \\ E[C'_k P_{k+1} B_k] & -\gamma^2 I + E[C'_k P_{k+1} C_k] \end{bmatrix}$$

$$526 \quad (4.33) \quad T_k = \begin{bmatrix} B' \\ C' \end{bmatrix} P_{k+1} A + \begin{bmatrix} \bar{B}' \\ \bar{C}' \end{bmatrix} P_{k+1} \bar{A}$$

$$527 \quad (4.34) \quad \Omega_k = I + B' P_{k+1} B + \sigma \bar{B}' P_{k+1} \bar{B}$$

$$528 \quad (4.35) \quad \Delta_k = -\gamma^2 I + E[C'_k P_{k+1} C_k]$$

$$529 \quad -E[B_k P_{k+1} C_k]' \Omega_k^{-1} E[B_k P_{k+1} C_k]$$

530 *Proof.* The necessity and sufficiency can be proved by applying the similar lines
 531 to Lemma 3.1 and Lemma 4.2, respectively, we thus omit them. \square

532 **Remark 4.5.** The result generalizes the deterministic H_∞ control theory in state
 533 space [14] and the idea is different from that of the existing literature [4] and [10].
 534 Specifically, [4] and [10] solved the H_∞ control problem for stochastic systems by
 535 obtaining the stochastic version of bounded real lemma. Moreover, [4] and [10] assume
 536 that the controller is linear state-feedback, and the results are given by linear matrices
 537 inequality.

538 **5. Further discussions.** In the section, we provide some explanations concern-
 539 ing the relationship between the achievable performance γ and the preview length d .
 540 The derivation of the necessary and sufficient condition in the last two sections offers
 541 some evidences supporting our explanations.

542 From Theorem 4.3, we know γ is determined by the constraint $\Delta_k < 0$. It
 543 together with (4.23) means that γ nonlinearly depends on all of coefficient matrices
 544 in the system and the weighted matrices in performance index.

545 According to (4.23), there holds

$$\begin{aligned}
546 \quad (5.1) \quad \Delta_k &= -\gamma^2 I + E[C'_{k+d} P_{k+d+1} C_{k+d}] \\
547 &\quad - E[B_{k+d} P_{k+d+1} C_{k+d}]' \Omega_{k+d}^{-1} E[B_{k+d} P_{k+d+1} C_{k+d}] \\
548 &\quad - C'_{k+d+1} \Delta_{k+d}^{-1} (P_{k+d+1}^{d-1})' C \\
549 &\quad - \sum_{f=1}^{d-1} (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{d-f} - (P_{k+1}^{d-1})' B \Omega_k^{-1} B' P_{k+1}^{d-1}
\end{aligned}$$

550 Since $\max_v \min_u J(k, N) \geq \min_u J(k, N)$ for any $v_i, i = k, \dots, N$ and a candidate of
551 $\min J_u(k, N) \geq 0$ with $v_i = 0, i = k, \dots, N$, $\max_v \min_u J(k, N) \geq 0$. It shows $P_k \geq 0$
552 and $\beta_k(i, i) \geq 0$. Associated with (4.25), there hold

$$\begin{aligned}
553 &\quad E[C'_{k+i+1} P_{k+i+2} C_{k+i+1}] \geq 0 \\
554 \quad E[C'_{k+i+1} P_{k+i+2} C_{k+i+1}] &\geq \sum_{f=0}^i (T_{k+1+f}^{i-f})' R_{k+1+f}^{-1} T_{k+1+f}^{i-f}
\end{aligned}$$

555 At the moment, it is direct that in order to guarantee that there exists $\gamma > 0$ such
556 that $\Delta_k < 0$ and

$$557 \quad (5.2) \quad \beta_{k+1}(d-1, d-1) > (P_{k+1}^{d-1})' B \Omega_k^{-1} B' P_{k+1}^{d-1}.$$

558 Observing Δ_k in Theorem 4.4 and Δ_k in Theorem 4.3, we find that there is
559 possibility to find a smaller γ for the H_∞ preview control problem than γ for the H_∞
560 control for delay-free stochastic systems since the last three terms appear in Δ_k in
561 (5.1).

562 An intuitive analysis is given from the game theory in the sequel. As the two play-
563 ers, the control u and the disturbance v try to minimize and maximize the performance
564 $J(0, N)$, respectively. The term $v'_k (T_{k+f}^{d-f})' R_{k+f}^{-1} T_{k+f}^{d-f} v_k$ can be regarded as the contribu-
565 tion of these two players' decision using the information v_k at instant $k+f$ to the
566 game value. This contribution will be very small in that they play the game. Yet the
567 player u contributes an additional value $v'_k (P_{k+1}^{d-1})' B \Omega_k^{-1} B' P_{k+1}^{d-1} v_k$ to the game value
568 at k instant, which may surpass the player v 's contribution $v'_k C'_{k+d+1} \Delta_{k+d}^{-1} (P_{k+d+1}^{d-1})'$
569 $C v_k$ at $k+d$ instant because v_k is the historical information at $k+d$ and plays a
570 increasingly weaker role as d increases. Based on this and (5.1), there are two conclu-
571 sions. One is that H_∞ preview control can suppress the external disturbance better
572 than the standard H_∞ full-information control, i.e. the former has a smaller distur-
573 bance suppression level γ . The other one is the dependence of achievable performance
574 on the preview length. Specifically, the larger the preview length d is, the smaller
575 γ is. Yet we should also notice that the performance γ may saturate for a certain
576 finite preview length, which may result from that the early historical information may
577 not be useful. Our two conclusions and the saturation phenomenon are supported by
578 Figure 1.

579 **6. Example.** In this section, we provide an example to illustrate the H_∞ control
580 for stochastic systems with disturbance preview.

581 Figure 1 [11] is a schematic of the quarter vehicle active suspension configuration.
582 It is broadly representative of the fundamental suspension problem of isolating the
583 vibration from the road. In this figure, m_s is the sprung mass, which represents
584 the vehicle chassis; m_u is the unsprung mass, which represents mass of the wheel

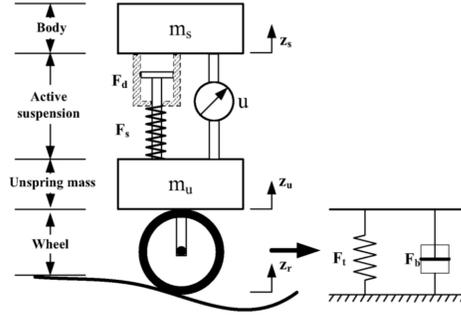


FIG. 1. the quarter vehicle active suspension

585 assembly; F_d and F_s are damping force and elastic force from the suspension system,
 586 respectively, and c_s and k_s are corresponding damping and stiffness, respectively; F_b
 587 and F_t are damping force and elastic force from the tire, respectively, and k_u and
 588 c_u stand for compressibility and damping of the pneumatic tyre, respectively; z_s and
 589 z_u are the displacements of the sprung and unsprung masses, respectively; u is the
 590 active input of the suspension system; z_r is the roadway elevation at vehicle, and it
 591 can be measured by the sensor mounting the suspension in advance and is thereby
 592 the same as that at the sensor position but delayed by a time (equal to the distance
 593 of the sensor in front of the vehicle divided by the vehicle velocity).

594 The dynamic equations of the sprung and unsprung masses are given by

595 (6.1) $m_s \ddot{z}_s + c_s(\dot{z}_s - \dot{z}_u) + k_s(z_s - z_u) = u$

596 (6.2) $m_u \ddot{z}_u + c_s(\dot{z}_s - \dot{z}_u) + k_s(z_s - z_u) + c_u(\dot{z}_u - \dot{z}_r) + k_u(z_u - z_r) = -u$

597 Define the following state variables:

598 (6.3) $x_1 = z_s - z_u$

599 (6.4) $x_2 = z_u - z_r$

600 (6.5) $x_3 = \dot{z}_s$

601 (6.6) $x_4 = \dot{z}_u$

602 where x_1 denotes the suspension deflection, x_2 is the tire deflection, x_3 is the sprung
 603 mass speed, and x_4 denotes the unsprung mass speed. We define disturbance input
 604 $v = \dot{z}_r$, which describes the roughness of the road. Then, by defining $x = [z_s -$
 605 $z_u, (\dot{z}_s - \dot{z}_u), \dot{z}_s, \dot{z}_u]'$, the dynamic equations in (6.1)-(6.2) can be rewritten in the
 606 following state-space form

607 (6.7) $\dot{x} = A_c x + B_c u + C_c v$

608 where

609 (6.8) $A_c = \begin{bmatrix} 0 & 0 & 1 & -1 \\ 0 & 0 & 0 & 1 \\ -\frac{k_s}{m_s} & 0 & -\frac{c_s}{m_s} & \frac{c_s}{m_s} \\ \frac{k_s}{m_u} & -\frac{k_t}{m_u} & \frac{c_s}{m_u} & -\frac{c_s+c_t}{m_u} \end{bmatrix}$

610 (6.9) $B_c = [0 \ 0 \ \frac{1}{m_s} \ -\frac{1}{m_u}]'$

611 (6.10) $C_c = [0 \ -1 \ 0 \ -\frac{c_t}{m_u}]'$

612 In designing the control law for a suspension system, we need to consider ride com-
 613 fort. It is widely accepted that ride comfort is closely related to the body acceleration.
 614 Therefore, when we design the controller, one of our main objectives is to reduce the
 615 body acceleration, that is, \dot{x}_3 . In addition, in order to make sure the vehicle safety,
 616 we should ensure the firm uninterrupted contact of wheels to road, and the dynamic
 617 tire load $k_t x_2$ should be small so that $|k_t x_2| < (m_s + m_u)g$. Because of mechanical
 618 structure, the suspension stroke x_1 should not exceed certain allowable maximum and
 619 it should be small either. Therefore, when we design the control law, our main ob-
 620 jective is to guarantee that the regulated signal $z = \left[\rho_1 \dot{x}_3 \quad \rho_2 \frac{k_t x_2}{(m_s + m_u)g} \quad \rho_3 x_1 \right]'$,
 621 a weighted column vector reflecting suspension body acceleration, the safety index
 622 (proportional to the tire deflection) and the body displacement (suspension stroke),
 623 is less than the weighted roughness of the road in the sense $\|z\| < \gamma \|v\|$, where
 624 $\rho_i \geq 0, i = 1, 2, 3$, are weights and are used for adjusting design preference. Now
 625 according to (6.7), z admits

$$626 \quad (6.11) \quad z = F_c x + D_c u$$

627 where

$$628 \quad (6.12) \quad F_c = \begin{bmatrix} -\rho_1 \frac{k_s}{m_s} & 0 & -\rho_1 \frac{c_s}{m_s} & \rho_1 \frac{c_s}{m_s} \\ 0 & \rho_2 \frac{k_t}{(m_s + m_u)g} & 0 & 0 \\ \rho_3 & 0 & 0 & 0 \end{bmatrix}$$

$$629 \quad (6.13) \quad D_c = \left[\rho_1 \frac{1}{m_s} \quad 0 \quad 0 \right]'$$

630 It is clear that system (6.7) has its matrices (A_c, B_c, C_c) depending on the physical
 631 parameters k_s, k_u, c_s, c_t, m_s . When they randomly deviates from their nominal val-
 632 ues as a result of oscillatory motion and the change with the operation conditions,
 633 k_s, k_u, c_s, c_t, m_s can be modeled as $k_s + w_{k_s}(t), k_u + w_{k_u}(t), c_s + w_{c_s}(t), c_t + w_{c_t}(t), m_s +$
 634 $w_{m_s}(t)$, here, $w_{k_s}(t), w_{k_u}(t), w_{c_s}(t), w_{c_t}(t), w_{m_s}(t)$ are independent white processes
 635 with variances $\sigma_{k_s}, \sigma_{k_u}, \sigma_{c_s}, \sigma_{c_t}, \sigma_{m_s}$, respectively. The simple derivation shows that
 636 $\frac{\sigma}{\sigma_{k_s}} w_{k_s}(t), \frac{\sigma}{\sigma_{k_u}} w_{k_u}(t), \frac{\sigma}{\sigma_{c_s}} w_{c_s}(t), \frac{\sigma}{\sigma_{c_t}} w_{c_t}(t), \frac{\sigma}{\sigma_{m_s}} w_{m_s}(t)$ are white processes with vari-
 637 ance σ . In particular, the approximation $\frac{1}{m_s + w_{m_s}(t)} \doteq \frac{1}{m_s} (1 - \frac{w_{m_s}(t)}{m_s})$ is used. This is
 638 the reason that we study the model with the multiplicative noise in this paper.

639 We borrow the quarter-vehicle suspension model parameters from [9] and list it in
 Table 1. Via the discretization of the vehicle suspension (6.7) and consideration of the

TABLE 1
 vehicle suspension parameters

m_s	m_u	k_s	c_s	k_t	c_t
973kg	114kg	42720N/m	101115N/m	1095Ns/m	14.6Ns/m

640

641 parameter random uncertainty mentioned above, we obtain a discrete time stochastic

642 system in the form of (2.1)-(2.2) with

643 (6.14)
$$A = \begin{bmatrix} 0.9251 & 0.1582 & 0.0176 & -0.0164 \\ 0.0669 & 0.8403 & 0.0022 & 0.0167 \\ -0.7711 & -0.2260 & 0.9722 & 0.0263 \\ 6.1633 & -14.8141 & 0.2248 & 0.6133 \end{bmatrix}$$

644 (6.15)
$$\bar{A} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0.0002 & 0 & 0.0004 & 0.0002 \\ 0.0002 & 0.0002 & 0.0004 & 0.0004 \end{bmatrix}$$

646 (6.16)
$$B = 10^{-3} \times \begin{bmatrix} 0.0018 \\ -0.0016 \\ 0.0180 \\ -0.1443 \end{bmatrix}, \bar{B} = \begin{bmatrix} 0 \\ 0 \\ 0.0001 \\ 0 \end{bmatrix}$$

647 (6.17)
$$C = \begin{bmatrix} -0.0011 \\ -0.0189 \\ 0.0015 \\ 0.1618 \end{bmatrix}, \bar{C} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0.003 \end{bmatrix}$$

648 (6.18)
$$F = \begin{bmatrix} -4.3905 & 0 & -0.1125 & 0.1125 \\ 0 & 0.9492 & 0 & 0 \\ 0.8 & 0 & 0 & 0 \end{bmatrix}, D = \begin{bmatrix} 0.001 \\ 0 \\ 0 \end{bmatrix}$$

649 where the sample period $T = 0.02$, and $\rho_1 = 0.1, \rho_2 = 0.1, \rho_3 = 0.8$.

650 In the following, applying the more general version of Theorem 4.3 to the system
 651 (2.1)-(2.2) with (6.14)-(6.18), we will illustrate the performance of the closed-loop
 652 discrete-time suspension system with disturbance preview and random parameter un-
 653 certainty. Evaluation of the vehicle suspension performance is based on the examina-
 654 tion of the sprung mass acceleration \dot{x}_3 (body acceleration), the safety index z_2 (tire
 655 deflection x_2), the sprung mass displacement x_1 (body displacement) and the H_∞
 656 level γ . A controller is to be designed such that the regulated signal z is bounded
 657 by the weighted disturbance. In order to evaluate the suspension characteristics with
 658 respect to ride comfort and safety, the variability of the road profiles is taken into
 659 account. In the context of the vehicle suspension performance, road disturbances can
 660 be generally assumed as shock. Shocks are events of relatively short duration and
 661 high intensity, caused by, for example, a pronounced bump or pothole on an other-
 662 wise smooth road. In the following, a kind of road profile is used to validate the
 663 performance of the presented control approach. Now consider the case of an isolated
 664 bump in an otherwise smooth road surface given by

665 (6.19)
$$z_r = \frac{A}{2}(1 - \cos(2\pi \frac{L}{V}t))$$

666 where A and L are the height and the length of the bump. Assume $A = 80mm, L =$
 667 $15m$ and the vehicle forward velocity $V = 45(km/h)$.

668 As Figure 2 shown, the random uncertainty deteriorates the suspension perfor-
 669 mance, in other word, the body acceleration z_1 , body displacement x_1 , safety index
 670 z_2 and the H_∞ performance γ increase as the random uncertainty of the suspension
 671 increases (i.e. σ becomes larger). On the other hand, the more the disturbance pre-
 672 view (larger d), the better the suspension performance, which means that the body

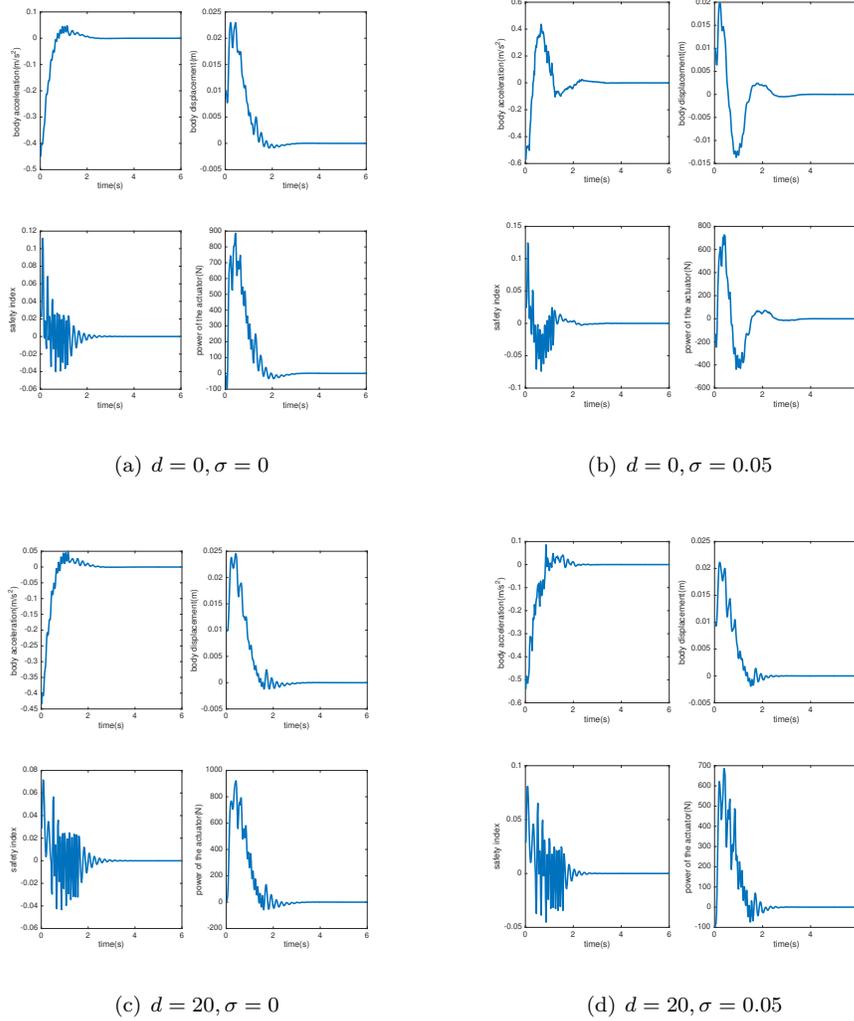


FIG. 2. Bump response of the vehicle active suspension

673 acceleration z_1 , body displacement x_1 , safety index z_2 and the H_∞ cost γ are smaller
 674 when more disturbance preview is utilized by the controller.

675 We also depict the curve of the optimal γ versus the preview length d for $N =$
 676 300 and several different σ in Figure 3. From Figure 3, the curve for $\sigma = 0$ is in
 677 agreement with the one provided by the method in [27]. Besides, we also observe two
 678 phenomena from Figure 3. One is the same conclusion as in Figure 2. The other is
 679 that using too much disturbance preview will not improve the suspension performance
 680 γ abidingly and the H_∞ performance will saturate after a certain length d .

681 **7. Conclusions.** In the paper, we obtain an analytic solution to the H_∞ preview
 682 control problem, which is an outstanding problem. It is shown that the problem is
 683 solvable if and only if a group of equations have solutions and an inertia condition
 684 holds. The proof depends heavily on how to characterize the necessary condition

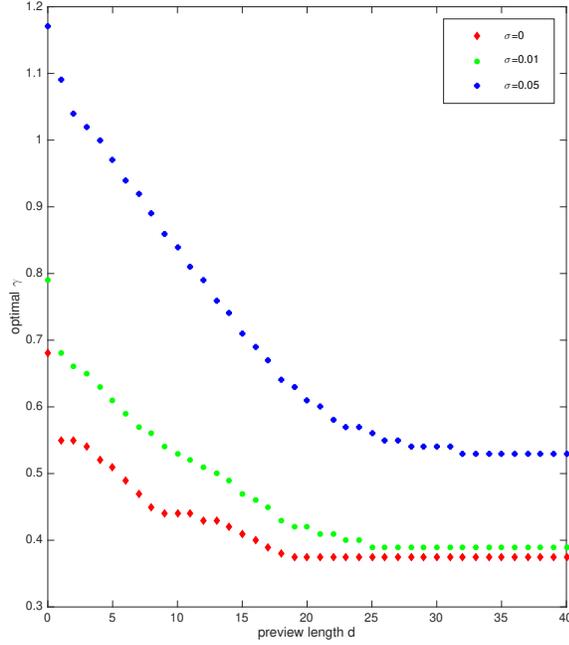


FIG. 3. Optimal H_∞ performance versus the length of preview in our example

685 better as the problem is solvable. We characterize it by a pair of stochastic difference
 686 equations with the aid of the projection principle in indefinite space which is helpful
 687 to get an explicit link between the two variables in the pair. The idea can also be
 688 used to solve the standard H_∞ control for stochastic systems completely and provide
 689 a solvability condition very similar to that for the deterministic counterpart. In fact,
 690 the idea can be applied to solve the game problems for stochastic systems with input
 691 delays too.

692 **Appendix A. Proof of Lemma 3.5.** We will present the proof of Lemma 3.5
 693 here by using dynamic programming, which provides an effective means of obtaining
 694 the optimal solution to the minimax problem by solving a sequence of static games
 695 in reverse time.

696 For using dynamic programming, we define a similar notation as in the proof of
 697 Lemma 3.1. Let

698 (A.1)
$$J(i, N) = \|z\|_{l_2[i, N]}^2 - \gamma^2 \|v\|_{l_2[i, N-d]}^2$$

699 Then

700 (A.2)
$$\begin{aligned} J(i, N) &= E\left[\sum_{k=i}^N z'_k z_k - \gamma^2 \sum_{k=i}^{N-d} v'_k v_k\right] \\ 701 &= E\left[\sum_{k=i}^N (x'_k F' F x_k + u'_k u_k) - \gamma^2 \sum_{k=i}^{N-d} v'_k v_k\right] \end{aligned}$$

702 In fact, in the case of $i > N - d$,

$$\begin{aligned}
703 \quad (\text{A.3}) \quad J(i, N) &= \|z\|_{l_{2[i, N]}}^2 \\
704 &= E \sum_{k=i}^N z'_k z_k \\
705 &= E \sum_{k=i}^N [x'_k F' F x_k + u'_k u_k]
\end{aligned}$$

706 since $\sum_{k=i}^{N-d} v'_k v_k = 0$.

707 With the same reason, if there is an adapted controller such that (2.5) holds for
708 some $\gamma > 0$, (3.2) is solvable. According to Lemma 3.1, the optimal u_k and v_k can be
709 characterized by (3.4) and (3.5). It should be stressed that the delay in disturbance
710 input v_k leads to a special characterization (3.5) of the optimal v_k , where there is a
711 time-lag between adapted processes v_k and λ_{k+d} . It will be very difficult to obtain
712 the solvability and the optimal inputs.

713 In order to re-express the optimal game value, we derive a relation as follows

$$\begin{aligned}
714 \quad (\text{A.4}) \quad & E[x'_k \lambda_{k-1} - x'_{k+1} \lambda_k] \\
715 &= E[x'_k (E[A'_k \lambda_k | \mathcal{F}_{k-1}] + F' F x_k) \\
716 &\quad - (A_k x_k + B_k u_k + C_k v_{k-d})' \lambda_k] \\
717 &= E[x'_k F' F x_k - (B_k u_k + C_k v_{k-d})' \lambda_k]
\end{aligned}$$

718 Applying (3.4) in the relation (A.4) leads to

$$\begin{aligned}
719 \quad (\text{A.5}) \quad & E[x'_k \lambda_{k-1} - x'_{k+1} \lambda_k] \\
720 &= E[x'_k F' F x_k - C'_k v'_{k-d} \lambda_k + u'_k u_k]
\end{aligned}$$

721 Adding from $k = n + 1$ to $k = N$ on the two sides of the equation (A.4), we have

$$\begin{aligned}
722 \quad (\text{A.6}) \quad & E[x'_{n+1} \lambda_n - x'_{N+1} \lambda_N] \\
723 &= \sum_{k=n+1}^N E[x'_k F' F x_k - C'_k v'_{k-d} \lambda_k + u'_k u_k]
\end{aligned}$$

724 Denote the optimal game value $\max_v \min_u J(n+1, N)$ as $J^*(n+1, N)$ and apply (3.5)
725 for $k \geq n+1$, then

$$726 \quad (\text{A.7}) \quad J^*(n+1, N) = E[x'_{n+1} \lambda_n] + \sum_{k=n+1}^{\min\{n+d, N\}} E[v'_{k-d} C'_k \lambda_k]$$

727 Let

$$728 \quad (\text{A.8}) \quad \bar{J}(n, N) = J^*(n+1, N) + z'_n z_n - \gamma^2 v'_n v_n$$

729 According to the dynamic programming principle, global optimization is the same
730 as local one, i.e. if $\max \min \|z\|_{l_{2[0, N]}}^2 - \|v\|_{l_{2[0, N-d]}}^2$ is solvable, $\max \min \|z\|_{l_{2[i, N]}}^2 -$
731 $\|v\|_{l_{2[i, N-d]}}^2$ is inevitably solvable, here $0 \leq i \leq N$. Moreover, the optimal solution of
732 the later is in accordance with the former's in the overlapped interval $[i, N]$. Hence,
733 $\bar{J}(n, N)$ is solvable over u_n, v_n .

734 With the above preparations, we now prove the three conclusions in the lemma
735 using the inductive method on k .

736 First consider the case of $k = N$. Applying (2.1), we have

$$\begin{aligned}
 737 \quad (\text{A.9}) \quad J(N, N) &= E[z'_N z_N + x'_{N+1} P_{N+1} x_{N+1}] \\
 738 &= E[x'_N (F'F + A'_N P_{N+1} A_N) x_N \\
 739 &\quad + u'_N (I + B'_N P_{N+1} B_N) u_N \\
 740 &\quad + v'_{N-d} C'_N P_{N+1} C_N v_{N-d} \\
 741 &\quad + 2x'_N A'_N P_{N+1} (B_N u_N + C_N v_{N-d}) \\
 742 &\quad + 2u'_N B'_N P_{N+1} C_N v_{N-d}]
 \end{aligned}$$

743 Because (3.2) is solvable, so is $\max_v \min_u J(N, N)$. Given that $J(N, N)$ only contains
744 a variable u_N to be determined, $\max_v \min_u J(N, N)$ actually becomes $\min_u J(N, N)$.
745 Hence, $E[I + B'_N P_{N+1} B_N] > 0$ and $R_N = \text{diag}\{E[I + B'_N P_{N+1} B_N], -\gamma^2 I\}$ has the
746 same inertias with Λ .

747 According to (3.4), the optimal u_N can be given as

$$\begin{aligned}
 748 \quad (\text{A.10}) \quad u_N &= -E[I + B'_N P_{N+1} B_N]^{-1} (E[B'_N P_{N+1} A_N] x_N \\
 749 &\quad + E[B'_N P_{N+1} C_N] v_{N-d})
 \end{aligned}$$

750 which associates with $v_N = 0$ shows (3.38) holds because of the facts $S_{N+1} =$
751 $0, P_{N+1}^j = 0, S_{N+1}^j = 0, j = 0, \dots, d-1$.

752 Inserting (A.10) and (2.1) into (3.6),

$$\begin{aligned}
 753 \quad (\text{A.11}) \quad \lambda_{N-1} &= E[A'_N \lambda_N | \mathcal{F}_{N-1}] + F' F x_N \\
 754 &= E[A'_N P_{N+1} (A_N x_N + B_N u_N \\
 755 &\quad + C_N v_{N-d}) | \mathcal{F}_{N-1}] + F' F x_N \\
 756 &= E[A'_N P_{N+1} (A_N x_N + C_N v_{N-d} \\
 757 &\quad - B_N E[I + B'_N P_{N+1} B_N]^{-1} (E[B'_N P_{N+1} A_N] x_N \\
 758 &\quad + E[B'_N P_{N+1} C_N] v_{N-d})) + F' F x_N \\
 759 &= (E[A'_N P_{N+1} A_N] + F' F - E[A'_N P_{N+1} B_N] \\
 760 &\quad \times E[I + B'_N P_{N+1} B_N]^{-1} E[B'_N P_{N+1} A_N]) x_N \\
 761 &\quad + (E[A'_N P_{N+1} C_N] - E[A'_N P_{N+1} B_N] \\
 762 &\quad \times E[I + B'_N P_{N+1} B_N]^{-1} E[B'_N P_{N+1} C_N] v_{N-d})
 \end{aligned}$$

763 The direct algebra calculation from (3.43)-(3.45), (3.46)-(3.48) and the initial matrices
764 values $S_{N+1} = 0, S_{N+1}^j = 0, P_{N+1}^j = 0, j = 0, \dots, d-1$ gives $P_N = E[A'_N P_{N+1} A_N] +$
765 $F' F - E[A'_N P_{N+1} B_N] E[I + B'_N P_{N+1} B_N]^{-1} E[B'_N P_{N+1} A_N], P_N^0 = (E[A'_N P_{N+1} C_N] -$
766 $E[A'_N P_{N+1} B_N] E[I + B'_N P_{N+1} B_N]^{-1} E[B'_N P_{N+1} C_N],$ and $P_N^j = 0, j = 1, \dots, d-1$.
767 Comparing them with (A.11), we can see that (3.39) holds as $k = N$.

768 What follows is to prove (3.40) holds for $k = N$. If the delay $d = 1$, then

$$769 \quad (\text{A.12}) \quad \lambda_{N+h-1} = \lambda_N = P_{N+1} x_{N+1}.$$

770 Plugging (2.1) and (A.10) into (A.12) yields

$$\begin{aligned}
 771 \quad (\text{A.13}) \quad \lambda_{N+d-1} &= P_{N+1} (A_N - B_N E[I + B'_N P_{N+1} B_N]^{-1} E[B'_N P_{N+1} A_N]) x_N \\
 772 &\quad + P_{N+1} (C_N B_N E[I + B'_N P_{N+1} B_N]^{-1} E[B'_N P_{N+1} A_N]) v_{N-d}
 \end{aligned}$$

773 which indicates that λ_{N+d-1} is in the form as (3.40) and the related coefficients only
774 involves w_N . If the delay $d > 1$, then

$$775 \quad (\text{A.14}) \quad \lambda_{N+d-1} = 0,$$

776 so it is trivial and (3.40) holds for $k = N$.

777 Inductively, assume those three conclusions in the lemma holds for all $k \geq n + 1$
778 , we will verify that those three conditions hold for $k = n$.

779 Since the case for $n \geq N - d$ is simpler and it can be handled with the similar
780 lines with the case for $n \leq N - d$, we assume $n \leq N - d$. Plugging (A.7), (3.6) with
781 $k = n$ and (2.1) in $\bar{J}(n, N)$ yields

$$\begin{aligned} 782 \quad (\text{A.15}) \quad \bar{J}(n, N) &= J^*(n+1, N) + z'_n z_n - \gamma^2 v'_n v_n \\ 783 &= E[x'_{n+1} \lambda_n] + \sum_{k=n+1}^{\min\{N, n+d\}} E[v'_{k-d} C'_k \lambda_k] \\ 784 &\quad + z'_n z_n - \gamma^2 v'_n v_n \\ 785 &= E[(A_n x_n + B_n u_n + C_n v_{n-d})' \\ 786 &\quad \times (P_{n+1} x_{n+1} + \sum_{i=0}^{d-1} P_{n+1}^i v_{n+1+i-d})] \\ 787 &\quad + \sum_{k=n+1}^{\min\{N, n+d\}} E[v'_{k-d} C'_k \lambda_k] \\ 788 &\quad + x'_n F' F x_n + u'_n u_n - \gamma^2 v'_n v_n \end{aligned}$$

789 As we focus on the quadratic term over the vector $\text{col}\{u_n, v_n\}$ in $\bar{J}(n, N)$, there holds

$$\begin{aligned} 790 \quad (\text{A.16}) \quad \bar{J}(n, N) &= E[(B_n u_n)'(P_{n+1} B_n u_n + P_{n+1}^{d-1} v_n)] \\ 791 &\quad + u'_n u_n + E[v'_n C'_{n+d} \lambda_{n+d}] - \gamma^2 v'_n v_n + \dots \\ 792 &= E[(B_n u_n)'(P_{n+1} B_n u_n + P_{n+1}^{d-1} v_n) \\ 793 &\quad + u'_n u_n - \gamma^2 v'_n v_n] \\ 794 &\quad + E[v'_n C'_{n+d} (S_{n+1} B_n u_n + S_{n+1}^{d-1} v_n)] \\ 795 &\quad + \dots \\ 796 &= E \begin{bmatrix} u_n \\ v_n \end{bmatrix}' R_n \begin{bmatrix} u_n \\ v_n \end{bmatrix} + \dots \end{aligned}$$

797 Observing the above expression, if the inertias of R_n is not equal to that of the matrix
798 $\text{diag}\{I, -\gamma^2 I\}$, one can come to a conclusion that $\max_v \min_u \bar{J}(n, N)$ is not solvable,
799 which conflicts with our previous result about it. Therefore, the inertia of R_n equals
800 to that of $\text{diag}\{I, -\gamma^2 I\}$ as $\max_v \min_u J(n, N)$ is solvable.

801 In light of (3.4)-(3.5) and the relation (3.39)-(3.40), there holds

$$802 \quad (\text{A.17}) \quad -u_n = E[B_n (P_{n+1} x_{n+1} + \sum_{j=0}^{d-1} P_{n+1}^j v_{n+1+j-d}) | \mathcal{F}_{n-1}]$$

$$803 \quad (\text{A.18}) \quad \gamma^2 v_n = E[C_{n+d} (S_{n+1} x_{n+1} + \sum_{j=0}^{d-1} S_{n+1}^j v_{n+1+j-d}) | \mathcal{F}_{n-1}]$$

804 Plugging (2.1) into them generates

$$805 \quad (A.19) \quad 0 = R_n \begin{bmatrix} u_n \\ v_n \end{bmatrix} + \begin{bmatrix} E[B'_n P_{n+1} A_n] \\ E[C'_{n+d} S_{n+1} A_n] \end{bmatrix} x_n$$

$$806 \quad + \sum_{j=1}^{d-1} \begin{bmatrix} E[B_n P_{n+1}^{j-1}] \\ E[C'_{n+d} S_{n+1}^{j-1}] \end{bmatrix} v_{n+j-d} + \begin{bmatrix} E[B'_n P_{n+1} C_n] \\ E[C'_{n+d} S_{n+1} C_n] \end{bmatrix} v_{n-d}$$

807 where we use the fact that S_{n+1} and S_{n+1}^j , $j = 0, \dots, d-1$ only involve the noises
 808 $\omega_{n+d}, \omega_{n+d-1}, \dots, \omega_{n+1}$. Now applying the notations (3.46)-(3.48), the optimal u_k, v_k
 809 admits (3.38).

810 In the sequel, we will verify the relationships (3.39)-(3.40) hold for $k = n$. By
 811 virtue of (3.6),

$$812 \quad (A.20) \quad \lambda_{n-1} = E[A'_n \lambda_n | \mathcal{F}_n] + F' F x_n$$

$$813 \quad (A.21) \quad \lambda_{n+d-1} = E[A'_{n+d} \lambda_{n+d} | \mathcal{F}_{n+d}] + F' F x_{n+d}$$

814 From the inductive assumption, (3.39)-(3.40) hold for $k = n+1$, consequently,

$$815 \quad (A.22) \quad \lambda_{n-1} = E[A'_n (P_{n+1} x_{n+1} + \sum_{j=0}^{d-1} P_{n+1}^j v_{n+1+j-d}) | \mathcal{F}_n] + F' F x_n$$

$$816 \quad (A.23) \quad \lambda_{n+d-1} = E[A'_{n+d} (P_{n+d+1} x_{n+1} + \sum_{j=0}^{d-1} P_{n+d+1}^j v_{n+1+j-d}) | \mathcal{F}_{n+d}] + F' F x_{n+d}$$

817 Substituting the system (2.1) with $k = n$ and the expression (3.38) of the optimal
 818 u_k, v_k with $k = n$ into the equality (A.22) and applying the recursive relations (3.43)-
 819 (3.45), one can derive that (3.39) holds for $k = n$. Apply (2.1) with $k = n, \dots, n+d-1$
 820 and (3.38) with $k = n, \dots, n+d-1$ in (A.23) until there only contain those terms over
 821 $x_n, v_{n-1}, \dots, v_{n-d}$ and then rearrange them, a relation like (3.40) can be obtained,
 822 and therein all of coefficient matrices indeed involve the noises $\{w_n, \dots, w_{n+d-1}\}$. At
 823 this moment, the case for $k = n$ has been clarified. The inductive proof is completed.

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